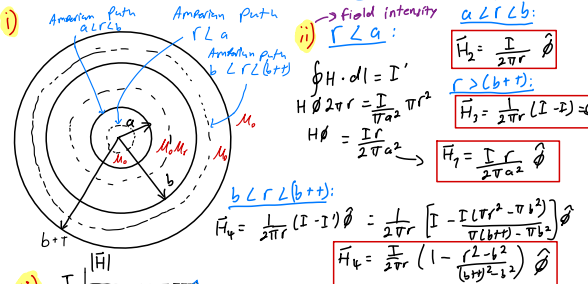


# Infinity Long Cable



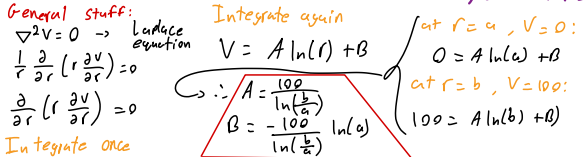
Field intensity  $H$  at radius  $r$ :

- Region 1 ( $a < r < b$ ):  $H_1 = \frac{I r}{2\pi a^2}$
- Region 2 ( $a > r > b$ ):  $H_2 = \frac{I}{2\pi r} \left(1 - \frac{r^2 - b^2}{(b^2 - a^2)}\right)$

Energy density  $w$  and total work done  $W$ :

- $w_1 = \frac{\mu_0}{2} H_1^2 = \frac{\mu_0 I^2 r^2}{4\pi^2 a^4}$  ( $a < r < b$ )
- $w_2 = \frac{\mu_0}{2} H_2^2 = \frac{\mu_0 I^2}{4\pi^2 r^2} \left(1 - \frac{r^2 - b^2}{(b^2 - a^2)}\right)^2$  ( $a > r > b$ )
- Total work done  $W = W_1 + W_2 = \frac{\mu_0 I^2 L}{4\pi} \left[ \frac{1}{4} + \mu_r \ln\left(\frac{b}{a}\right) \right]$
- Capacitance  $C = \frac{2\pi \epsilon_0 L}{\ln(b/a)}$

# Laplace - Dielectric



General stuff:  $\nabla^2 V = 0$  (Laplace equation)

Integrate again:  $V = A \ln(r) + B$

Boundary conditions:  $V=0$  at  $r=a$ ,  $V=100$  at  $r=b$

Solution:  $V(r) = \frac{100}{\ln(b/a)} \ln\left(\frac{r}{a}\right)$

Electric field intensity  $E = -\nabla V = -\frac{100}{r \ln(b/a)} \hat{r}$

Charge density  $\rho_s = |\nabla \cdot \epsilon \mathbf{E}| = \frac{400 \epsilon_0}{r \ln(b/a)}$

Capacitance  $C = \frac{Q}{V} = \frac{8\pi \epsilon_0 L}{\ln(b/a)}$

Leakage resistance  $R = \frac{L}{\sigma C} = \frac{4 \epsilon_0}{\sigma \ln(b/a)}$

# Generic formulas

Volume element  $dV = R^2 \sin\theta dr d\theta d\phi$

Surface element  $dS = R^2 \sin\theta d\theta d\phi$

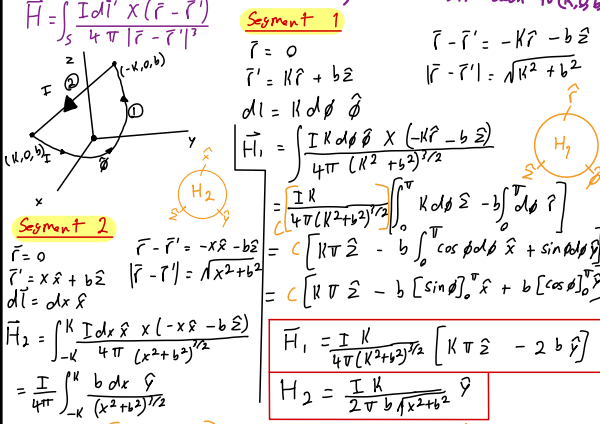
Line element  $dL = R d\phi$

Point of observation  $\vec{r}$

Generic point on a source  $\vec{r}'$

Trigonometric identities:  $\sin^2\theta + \cos^2\theta = 1$ ,  $\sin 2\theta = 2 \sin\theta \cos\theta$ ,  $\cos 2\theta = \cos^2\theta - \sin^2\theta$ ,  $\sin(\theta \pm \phi) = \sin\theta \cos\phi \pm \cos\theta \sin\phi$ ,  $\cos(\theta \pm \phi) = \cos\theta \cos\phi \mp \sin\theta \sin\phi$

# Biot - Savart

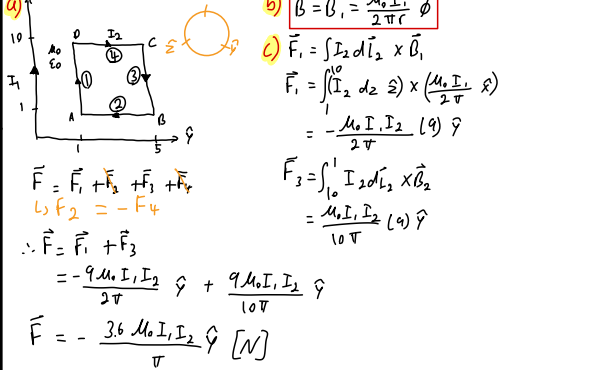


Segment 1:  $\vec{H}_1 = \int \frac{I d\vec{l} \times (\vec{r} - \vec{r}')}{4\pi |\vec{r} - \vec{r}'|^3}$

Segment 2:  $\vec{H}_2 = \int \frac{I d\vec{l} \times \hat{r}}{4\pi r^2}$

Final results for the semi-circle filament:  $H_1 = \frac{IK}{4\pi \sqrt{K^2 + b^2}} [K\pi - 2b\psi]$ ,  $H_2 = \frac{IK}{2\pi b \sqrt{K^2 + b^2}}$

# Infinity Long Filament



Force on filament due to  $I_{loop}$ :  $F_N = -F$

Final force:  $F_N = \frac{3.6 \mu_0 I_1 I_2}{\pi} \psi [N]$

# Generic Questions

## Maxwell Equations

Gauss' Law $\nabla \cdot \vec{E} = \frac{\rho}{\epsilon_0}$	$\nabla \cdot \vec{D} = \rho_v$	$\oint_S \vec{D} \cdot d\vec{s} = Q$
Maxwell-Faraday $\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$	$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$	$\oint_C \vec{E} \cdot d\vec{l} = -\int_S \frac{\partial \vec{B}}{\partial t} \cdot d\vec{s}$
Gauss' Law for Magnetism $\nabla \cdot \vec{B} = 0$	$\nabla \cdot \vec{B} = 0$	$\oint_S \vec{B} \cdot d\vec{s} = 0$
Ampere Circuit $\nabla \times \vec{H} = \vec{J} + \epsilon_0 \frac{\partial \vec{E}}{\partial t}$	$\nabla \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t}$	$\oint_C \vec{H} \cdot d\vec{l} = \int_S (\vec{J} + \frac{\partial \vec{D}}{\partial t}) \cdot d\vec{s}$

## Continuity of Current

Point form:  $\nabla \cdot \vec{J} = -\frac{\partial \rho_v}{\partial t}$  Integral form:  $I_{out} = \int_S \frac{\partial \vec{D}}{\partial t} \cdot d\vec{s}$

## Displacement Current density

$\nabla \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t} \Rightarrow \int_C (\vec{H} \cdot d\vec{l}) = \int_S \vec{J} \cdot d\vec{s} + \int_S \frac{\partial \vec{D}}{\partial t} \cdot d\vec{s}$

Stokes:  $\oint_C \vec{H} \cdot d\vec{l} = I_c + \int_S \frac{\partial \vec{D}}{\partial t} \cdot d\vec{s}$   
 $\therefore I_D = \int_S \vec{J}_D \cdot d\vec{s} = \int_S \frac{\partial \vec{D}}{\partial t} \cdot d\vec{s} \therefore I_D = \frac{\partial Q}{\partial t}$

## Mechanisms that cause EMI with 3 fixes

- |                        |                                  |
|------------------------|----------------------------------|
| Mechanism:             | fixes:                           |
| - ground               | - shielding                      |
| - Antenna effect       | - filtering and grounding        |
| - cross talk           | - layout and component placement |
| - switching operations |                                  |
| - Differential mode    |                                  |

## Magnetic Boundary $\mu_1 = \mu_0, \mu_2 = 500\mu_0$

Normal direction  $\hat{n} = \hat{r}$   
 → normal/tangential component of magnetic flux

a)  $\vec{B}_{2n} = \vec{B}_2 \cdot \hat{n} = 15$   
 $\vec{B}_{2n} = 15\hat{r} \quad \vec{B}_{2t} = 100\hat{\phi} + 250 \cos \phi \hat{z}$

b) → find  $B_2$  with  $\vec{B}_2 = 15\hat{r} + 100\hat{\phi} + 250\hat{z}$   
 $\vec{B}_2 \cdot \hat{n} = 15 \quad \hat{n} \times (\vec{H}_1 - \vec{H}_2) = \vec{J}_s$   
 $\vec{H}_1 \times \hat{r} = \vec{J}_c + \vec{H}_2 \times \hat{r}$   
 $= -J_0 \hat{z} + \frac{\mu_2}{\mu_1} \vec{H}_2 \times \hat{r}$   
 $= -J_0 \hat{z} + \frac{15\hat{r} \times \mu_2}{\mu_1} + \frac{100\hat{\phi} \times \mu_2}{\mu_1} + \frac{250\hat{z} \times \mu_2}{\mu_1}$

$(H_{1r}\hat{r} + H_{1\phi}\hat{\phi} + H_{1z}\hat{z}) \times \hat{r} = -J_0 \hat{z} - \frac{100\hat{z}}{\mu_2} + \frac{250\hat{\phi}}{\mu_2}$   
 $-H_{1\phi}\hat{z} + H_{1z}\hat{\phi} = -J_0 \hat{z} - \frac{100\hat{z}}{\mu_2} + \frac{250\hat{\phi}}{\mu_2}$   
 $H_{1\phi} = J_0 + \frac{100}{\mu_2} \quad H_{1z} = \frac{250}{\mu_2}$   
 $\vec{H}_1 = (J_0 + \frac{100}{\mu_2})\hat{\phi} + \frac{250}{\mu_2}\hat{z}$   
 $\vec{B}_1 = \mu_1 \vec{H}_1 = (\mu_1 J_0 + \frac{100}{500})\hat{\phi} + \frac{250}{500}\hat{z}$   
 $= (\mu_1 J_0 + 0.2)\hat{\phi} + 0.5\hat{z}$

$\vec{B}_1 = 15\hat{r} + (\mu_1 J_0 + 0.2)\hat{\phi} + 0.5\hat{z}$

c) → find  $B_1$  with  $\vec{B}_2$  at  $\phi = 90^\circ \quad \vec{B}_2 = 15\hat{r} + 100\hat{\phi}$

$\vec{B}_{2n} = 15\hat{r} = \vec{B}_{1n}$   
 $\vec{B}_{2t} = 100\hat{\phi}$   
 $\vec{H}_{2t} = \vec{H}_{1t} \Rightarrow \frac{B_{2t}}{\mu_2} = \frac{B_{1t}}{\mu_1}$   
 $\vec{B}_{1t} = \frac{\mu_1}{\mu_2} \vec{B}_{2t} = \frac{\mu_0}{500\mu_0} 100\hat{\phi} = 0.2\hat{\phi}$   
 $\vec{B}_1 = 15\hat{r} + 0.2\hat{\phi} \text{ at } \hat{\phi} = 0$

# Stationary Loop

$x-y$  plane,  $a = 0.5m$   
 $R_1 = 0.4\Omega, R_2 = 400\Omega, \omega = 10^6 \text{ rad/s}$   
 $\vec{B}(t) = 6(3\hat{r} - 5r\hat{z}) \cos \omega t \quad Wb/m^2$

a)  $\phi = \int \vec{B}(t) \cdot d\vec{s}$   
 $= \int_{r=0}^{2\pi} \int_{\phi=0}^a (18\hat{r} - 30r\hat{z}) \cos \omega t \cdot r \, d\theta \, dr \, dz$   
 $= 180 \cos(\omega t) \int_0^a r^2 dr \int_0^{2\pi} d\theta$   
 $= \frac{180\pi (0.5)^3}{3} \cos(10^6 t)$

$\phi = \frac{5\pi}{2} \cos(10^6 t)$

b)  $V_{emf}^{tr} = -\int \frac{\partial \vec{B}}{\partial t} \cdot d\vec{s}$   
 $= -\int_S \frac{\partial}{\partial t} (18\hat{r} - 30r\hat{z}) \cos \omega t \cdot r \, dr \, d\theta \, dz$   
 $= +\int_S \omega \sin \omega t (18\hat{r} - 30r\hat{z}) \cdot r \, dr \, d\theta \, dz$   
 $= \omega \sin \omega t (18\hat{r} - 30\int_0^a r^2 dr) \int_0^{2\pi} d\theta$   
 $= \frac{30 \times (0.5)^3}{3} \times 2\pi \omega \sin \omega t = 2.5 \sin \omega t$

d) Set  $\omega = 10^6$  and  $\omega t = \frac{5\pi}{4}$   
 $V_{emf}^{tr} = -1.76 \times 10^6 V$   
 $I = \frac{V_{emf}^{tr}}{R} = \frac{V_1 - V_2}{400} = \frac{-1.76 \times 10^6}{400}$   
 $I = -4.42$  in counter clockwise

## Moving Loop in Static field $u = -10\hat{r} \text{ m/s}$

a)  $B$  at  $\gamma_1 \Rightarrow B(\gamma_1) = 5 \cos(0.1 \times 4) \hat{z}$   
 $\therefore B(\gamma_1) = 4.605 \text{ Wb/m}^2$

b)  $V_{12} = V_{emf} = \int \vec{u} \times \vec{B} \cdot d\vec{l}$   
 $= \int_1^2 (-10\hat{r} \times 4.605\hat{z}) \cdot d\vec{l} \hat{x}$   
 $V_{12} = 92.1 V$

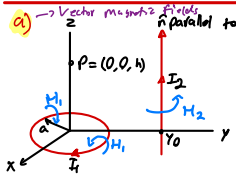
c)  $B$  at  $\gamma_2 \Rightarrow B(\gamma_2) = 5 \cos(0.1 \times 4.5) \hat{z}$   
 $B(\gamma_2) = 4.502 \hat{z} \text{ Wb/m}^2$

d)  $V_{43} = \int (-10\hat{r} \times 4.502\hat{z}) \cdot d\vec{l} \hat{x}$   
 $V_{43} = 90.04 V$

e)  $V_{41} = V_{32} = 0$

f)  $I = \frac{V_{12} - V_{43}}{R} = \frac{92.1 - 90.04}{25} = \frac{1.7}{25}$  counter clockwise

# Magnetic field of a wire



a) → Vector magnetic fields  
 $\vec{H}$  parallel to  $\hat{z}$

b) → Find Magnetic field  $H$   
 for  $I_2$ :  

$$\vec{H}_2 = \frac{I_2}{2\pi Y_0} \hat{\phi}$$

$$= \frac{I_2}{2\pi Y_0} [-\sin\phi \hat{x} + \cos\phi \hat{y}] \quad \phi = \frac{\pi}{2}$$

$$\vec{H}_2 = \frac{I_2}{2\pi Y_0} \hat{x}$$

c) → find  $H$  given  
 $Y_0, a, b, I_1, I_2$

$$H = -\frac{2a \times 5^2}{2(5^2 + a^2)^{3/2}} + \frac{3a}{2\sqrt{(2a)}} \quad [A/cm]$$

for  $I_1$ :  
 $\vec{r} = h \hat{z}$   
 $\vec{r}' = a \hat{r}$   
 $\vec{r} - \vec{r}' = h \hat{z} - a \hat{r}$   
 $|\vec{r} - \vec{r}'| = \sqrt{h^2 + a^2}$   
 $I_1 dl = I_1 a d\phi$

$$\vec{H}_1 = \int \frac{I_1 dl \times (\vec{r} - \vec{r}')}{4\pi |\vec{r} - \vec{r}'|^2}$$

$$= \frac{-I_1 a}{4\pi (a^2 + h^2)^{3/2}} \int_0^{2\pi} [h d\phi \hat{r} + \int_0^{2\pi} a d\phi \hat{z}]$$

$$= \frac{-I_1 a}{4\pi (a^2 + h^2)^{3/2}} (a(2\pi) \hat{z})$$

$$\vec{H}_1 = \frac{-I_1 a^2}{2(a^2 + h^2)^{3/2}} \hat{z}$$

d)  $\vec{F} = I \vec{l} \times \vec{B}$   
 $\vec{F} = I \oint dl \times \vec{B}$

$$\vec{H} = \vec{H}_1 + \vec{H}_2$$

## Ampere's Law for cylinder

a)  $\oint \vec{H}_1 \cdot d\vec{l} = \int \vec{J} \cdot d\vec{s}$

$$\Rightarrow H \phi 2\pi r = \int \vec{J}_0 \cdot e^{-r} \hat{z} \cdot r dr d\phi d\hat{z}$$

$$H \phi 2\pi r = J_0 \int_0^r e^{-r} dr \int_0^{2\pi} d\phi$$

$$H \phi r = -J_0 (e^{-r} - 1)$$

$$\vec{H}_1 = \frac{-J_0}{r} (1 - e^{-r}) \hat{\phi}$$

b) 
$$H_2 = \frac{J_0}{r} (1 - e^{-a}) \hat{\phi}$$

c)  $|H_1| = \frac{3}{5} (1 - e^{-5})$   
 $|H_2| = \frac{3}{5} (1 - e^{-5})$  ← Same

